

## FIBRE-OPTIC SURVEILLANCE SYSTEM

The present invention relates to fibre-optic surveillance systems, particularly fibre-optic perimeter surveillance systems.

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It is known to use optical fibres as sensing elements to detect pressure, strain etc, with conditions external to an optical fibre being inferred from changes in characteristics, such as amplitude, frequency or polarisation, in light output from the fibre. An example is the pressure sensor described in European Patent 10 number 0 365 062.

One approach to perimeter surveillance is to arrange a single length of optical fibre below ground level around a perimeter to be monitored, and to couple radiation from an LED or laser-diode into the fibre. Pressure on the fibre due to the weight 15 of a person, vehicle or other object crossing a perimeter defined by the fibre causes a change in the amount of radiation back-scattered within the fibre (due to bending of the fibre), and hence the presence of an intruder can be detected. However, such a system has three significant disadvantages, namely (i) the position at which an intruder crosses the perimeter cannot be determined 20 accurately, (ii) a significant false-alarm rate, (iii) no information is given about the nature if the intruding person or object and (iv) an inability to multiplex multiple sensing zones on a single fibre. Alternatively, the transmission of the fibre may be monitored as described in US patent 4 812 645. This types of system has similar drawbacks.

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Optical fibre interferometric sensors can be used to detect pressure and vibration. When a length of optical fibre is subjected to an external pressure the fibre is deformed. This deformation alters the optical path length of the fibre, which can be detected as a change in phase of light passing along the fibre. As it is possible

5 to analyse for very small changes in phase, optical fibre sensors are extremely sensitive to applied pressure. Such a sensor is described as an interferometric sensor. This high sensitivity allows optical fibre sensors to be used for example, in acoustic hydrophones where sound waves with intensities equivalent to a pressure of  $10^{-4}$  Pa are routinely detectable. Published UK patent application 2 262 803

10 describes an interferometric system having a serial array of distributed fibre-optic sensors, however such a system provides no accurate positional information about an intruder or information relating to the nature of the intruder.

Published UK patent application 2 176 364 discloses a serial array of localised

15 fibre-optic sensors. This system is only able to provide detection if an intruding person, vehicle etc passes one of the localised sensors.

According to a first aspect of the invention, these problems are ameliorated by a

20 fibre-optic sensor array for a surveillance system characterised in that the sensor array comprises at least two fibre-optic point sensors, in which each pair of successive point sensors are linked by a distributed fibre-optic sensor.

Optical fibre sensors have the advantage that they can be multiplexed without recourse to local electronics. Interferometric sensors can also be formed into

25 distributed sensors with a length sufficient to cover that of typical security zone

perimeters (20-100m). By adopting this hybrid approach of point sensors and interstitial distributed sensors the system benefits from a high detection efficiency.

A second aspect of the invention provides a fibre-optic surveillance system  
5 characterised in that the system comprises a fibre optic sensor of the invention connected to an interrogation system adapted to respond to an optical phase shift in at least one sensor of the array due to a force applied to that sensor and to establish the position the position at which said force is applied.

10 The force could be applied by a person, animal, vehicle or other object crossing a path which is under surveillance, with the sensor array being positioned on or near the path, or underneath it.

This provides a low cost, reliable fibre-optic surveillance system which is suitable  
15 for perimeter monitoring and which can be highly multiplexed. Remote interrogation is possible so neither local electronics nor local electrical power are required.

20 The fibre-optic sensor array may be connected to the interrogation system by a fibre-optic cable or alternatively by a transducer and a wire cable.

The fibre-optic point sensors may comprise optical fibre wound into a flexural disc, or may for example be geophones.

25 Alternatively the fibre-optic point sensors may be fibre-optic accelerometers. The need to monitor extremely low levels of vibration in security and seismic survey

has spurred the development of ever more sensitive accelerometers. Fibre optic technology has been applied to this particular field in the form of fibre-optic accelerometers based on interferometric techniques. The compliant cylinder approach to the design of a fibre-optic accelerometer is particularly effective when  
5 incorporated in such an interferometer. In one known approach a seismic mass is held in place by two compliant cylinders and around the circumference of each cylinder there being wound a single mode optical fibre, which form the arms of an interferometer. In another approach, a single compliant cylinder loaded with a seismic mass is wound circumferentially with an optical fibre.

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The distributed fibre optic sensors preferably comprise optical fibre packages for measuring pressure on, or bend, of the distributed sensors.

Preferably, the interrogation system comprises a reflectometric interferometric  
15 interrogation system, more preferably the interferometric interrogation system comprises a pulsed reflectometric interferometric interrogation system in which Time Division Multiplexing (TDM) is used to distinguish individual sensors. This is a very efficient multiplexing architecture that can be used with distributed and point sensors. Furthermore wavelength Division multiplexing (WDM) can be used to  
20 increasing the number of sensors multiplexed on a single fibre further.

Alternatively, the interferometric interrogation system may comprise a Rayleigh backscatter interferometric interrogation system, with a pulsed Rayleigh backscatter interferometric interrogation system being particularly preferred.

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A non-Rayleigh backscattering reflectometric system relies upon discrete reflectors between sensors. These are comparatively expensive components, which may add to the cost of the overall system. In contrast, Rayleigh backscattering relies on reflection of light from inhomogeneities in the optical fibre.

- 5 This removes the need for discrete reflectors, reducing the overall cost of the system. However, the data collected from such a system requires more complex analysis than a reflectometric interrogation system.

A third aspect of the invention provides a method of establishing the position at  
10 which an object moving on the earth's surface crosses a closed path, or an open path of fixed length, thereon, characterised in that the method comprises the steps of

- (i) positioning a sensor according to claim 1 on or below said path; and  
15 (ii) analysing optical signals received from the sensor to establish the position of the object along the path, or the position at which the object has crossed said path.

The optical signals are preferably analysed by measuring the delay between the signals received from adjacent fibre-optic point sensors along the array and  
20 combining these signals with the signal from the distributed fibre-optic array linking those fibre-optic point sensors to locate and confirm the said position.

An embodiment of the invention are described below by way of example only and with reference to the accompanying drawing in which schematically illustrates a  
25 fibre-optic perimeter surveillance system according to the invention.

In Figure 1, a fibre-optic perimeter surveillance system according to the invention is indicated generally by 10. The system 10 comprises a series of fibre-optic point sensors 16A, 16B, 16C, 16D, ....., 16N (in this example, geophones) optically linked by a series of distributed fibre-optic sensors 18B, 18C, 18D, ....., 18N to form a fibre-optic sensor array 15. A data link 14 couples the geophone 16A to an interrogation unit 12. The data link 14 may be a length of optical fibre, so that optical signals are passed to the interrogation unit 12, or alternatively it may comprise a detector which converts optical signals into electrical signals and either a fixed electrical, or wireless, link to the interrogation unit 12.

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The distributed fibre-optic sensors 18B, 18C, 18D, ....., 18N each have a physical length of 100m. There are 250 geophones in the array 15, so that the separation of geophones 16A, 16N may be up to approximately 24.9km.

15    Each of the geophones 16A, 16B, 16C, 16D, ....., 16N comprises approximately 100m of optical fibre wound onto a flexural disc, and is able to measure acceleration and displacement via strain induced in the fibre. Each of the distributed sensors 18B, 18C, 18D, ....., 18N comprises 100m of optical fibre packaged within a cable and can measure pressure on, or bend of, the cable, also  
20    via strain induced on the fibre.

The array 15 may be arranged in any desired configuration, for example it may be arranged around a closed path to provide perimeter surveillance for e.g. a building; alternatively it may be arranged in a linear manner to provide information on the  
25    location of a person/object crossing a straight line defined by the array 15.

- The system 10 operates as follows. When a person or object crosses a line or perimeter on or underneath which the array 15 is positioned, a force resulting from the person's or object's weight (plus possibly also a force resulting from a change in momentum if there is an impact) is applied to the sensor array. This causes
- 5 radiation within a distributed fibre-optic sensor corresponding to the location where the person/object crosses to be reflected back to geophone 16A and a corresponding signal giving approximate location is passed to the interrogation unit 12. More particularly the interrogation unit 12 is able to identify that a crossing has occurred somewhere along the length of the array 15. Radiation is also
- 10 reflected back from the geophones at either end of that distributed sensor, and corresponding signals are also passed to the interrogation unit 12. The interrogation unit 12 carries out triangulation of the signals received from the distributed sensor and the geophones at either end of it to accurately determine the location along the array 15 at which the person/object has crossed on the
- 15 basis of the time at which signals are received. By using data from both types of sensor, it is possible to provide much more accurate classification of the person/object than is achievable through use of one sensor type alone. Improved classification results in a lower false-alarm rate.
- 20 In the example system 10, the point fibre-optic sensors are geophones, however other types of fibre-optic point sensor may be used.
- The number of point and distributed sensors may vary according to both the length of a perimeter or path which is desired to be monitored, and the accuracy with
- 25 which it is desired to locate intruder events. The simplest fibre-optic sensor of the

invention would comprise a single distributed sensor having a point sensor at each end.

Given that the detection range of a person walking using a ground mounted fibre  
5 optic accelerometer can be >30m in certain ground types, an array of accelerometers positioned say 40m apart will ensure full coverage of a perimeter.

By comparing signals received on adjacent accelerometers and measuring the time difference between common features on the signal it is possible to accurately  
10 calculate the position of the intrusion along the length of the interstitial fibre.

Further temporal and frequency analysis of the accelerometer signals and the singles received from the distributed interstitial sensing cable enable intrusion classification , thereby reducing the system false alarm rate.

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Suitably, the known distance is between 20m and 50m. The known distance refers to the physical separation of the fibre optic sensors and is defined by the optical path length of the optical fibre between each sensor and the length of fibre used in each accelerometer.

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